# STOCHASTIC COMPLEXITY FOR THE ESTIMATION OF SINE-WAVES IN COLORED NOISE

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#### ABSTRACT

During recent years the advances in stochastic complexity (SC) have led to new exact formulae or to sharper approximations for large classes of models. We focus on the use of the SC to estimate the structure for the model of sine-waves in Gaussian autoregressive noise. Since the evaluation of SC relies on the determinant of the Fisher information matrix (FIM), the computation of FIM is revisited. It is shown for small and moderate sample sizes that SC compares favorably with other well-known criteria such as: BIC, KICc and GAIC.

*Index Terms*— Minimum Description Length principle, sinusoidal regression, autoregressive processes, structure selection, Fisher information matrix.

## 1. INTRODUCTION AND PRELIMINARIES

We address the estimation of the number of sinusoidals observed in additive noise with unknown correlation structure. To formulate the problem, we consider the data model

$$y_t = x_t + e_t, t \in \{0, \dots, N-1\}, x_t = \sum_{k=1}^{K} \alpha_k \cos(\omega_k t + \phi_k),$$
(1)

where  $y_t$  denotes the measurements,  $x_t$  is the noise-free signal and  $e_t$  is the colored Gaussian noise.

To ensure the identifiability of the parameters, we assume as usual that the amplitudes  $\alpha_k$  are strict positive and the frequencies  $\omega_k$  belong to the interval  $(0, \pi)$ . The frequencies are distinct and, without loss of generality,  $\omega_1 < \cdots < \omega_K$ . Both the amplitudes and the frequencies are non-random parameters that will be estimated from the available measurements.

Two different hypotheses will be considered for modeling the phases  $\phi_k \in [-\pi, \pi)$ :  $H_{dp}$  - the phases are unknown deterministic constants;  $H_{rp}$  - the phases are independent and uniformly distributed random variables that are also independent of  $e_t$ . For both assumptions, the statistical properties of  $y_t$  have been investigated in previous studies, and more details can be found, for example, in [1].

In line with the approach from [1][2][3] and the references therein, we model the noise  $e_t$  as a stable autoregressive (AR) process with order M:

$$e_t = -\sum_{m=1}^M a_m e_{t-m} + w_t,$$
 (2)

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where  $w_t$  is a sequence of independent and identically distributed Gaussian random variables with zero mean and variance  $\tau$ . Since we consider only the case of real sinusoidals in real AR noise, we emphasize that the white random process  $w_t$  and the coefficients  $a_m$ ,  $1 \le m \le M$ , are real-valued.

Recall the definition of the local SNR for the k-th sinusoid,  $\text{SNR}_k = \frac{\alpha_k^2/2}{\tau/|A(\omega_k)|^2}$ , where  $A(\omega_k) = 1 + \sum_{m=1}^M a_m \exp(-jm\omega_k)$ and  $j = \sqrt{-1}$  [4].

Based on (1) and (2), we note that the parameters of the model are  $\tau$  and  $\theta = (\xi, \mathfrak{a})$ , where  $\xi = (\xi_1, \ldots, \xi_K)$  with the convention  $\xi_k = (\alpha_k, \omega_k, \phi_k)$  for the k-th sine-wave. The notation  $\mathfrak{a}$  is employed for the set of the AR coefficients  $(a_1, \ldots, a_M)$ .

Because the model structure  $\gamma = (K, M)$  is not known a priori, we resort to the traditional model selection procedure that comprises two steps: (a) for all pairs of integers  $\gamma = (K, M)$  that satisfy  $0 \le K \le K_{max}$  and  $0 \le M \le M_{max}$ , estimate the model parameters  $\hat{\theta}_{\gamma}$  from the observations  $y^N = y_0, \ldots, y_{N-1}$ ; (b) evaluate an information theoretic criterion for all  $\gamma$ s considered at the first step, and choose the model structure  $\hat{\gamma}$  that minimizes the criterion.

The most popular information theoretic rules for order selection can be reduced to a common form with two terms, where the first one is given by the minus maximum log-likelihood. The second term is a penalty coefficient that depends on the number of parameters of the model and, for some criteria, also on the sample size N [5]. In general, the selection rules used in practical applications are derived for  $N \rightarrow \infty$ , and the asymptotic approximations could potentially yield false conclusions when the sample size is small or moderate.

During recent years, the advances in stochastic complexity (SC) have led to new exact formulae or to sharper approximations for large classes of models [6][7][8], but the use of the new results in signal processing is scarce. We illustrate next how SC can be applied to estimate the structure for the model of sine-waves in Gaussian AR noise.

The rest of the paper is organized as follows. Section 2 is focused on the SC formula for sinusoids in AR noise. Because the evaluation of SC relies on the determinant of the Fisher information matrix (FIM), the computation of FIM is revisited in Section 3. SC and three other well-known criteria are compared in Section 4 to evaluate their performances in estimating the number of sinusoids from simulated data.

#### 2. SC FOR SINE-WAVES IN AR NOISE

Under mild assumptions on the maximum likelihood (ML) estimates  $\hat{\theta} = \hat{\theta}(y^N)$  and  $\hat{\tau} = \hat{\tau}(y^N)$ , we can use the expression of SC given

in [6]. We employ the notation  $f(y^N; \theta, \tau)$  for the likelihood function of  $y^N$ , thus  $\ln f(y^N; \hat{\theta}, \hat{\tau})$  is the maximum log-likelihood.  $\Theta$  denotes the parameter space and  $\mathbf{J}_N(\theta) = E\left[-\frac{\partial^2 \ln f(y^N; \theta, \tau)}{\partial \theta \partial \theta^{\top}}\right]$  is the Fisher information matrix (FIM).

It is well-known that the SC derivation is grounded in information theory. The predictive approach treats the white noise variance  $\tau$  as a nuisance parameter in the sense that the code length to describe it is not included in the SC formula. In our application, we noticed that considering the cost for transmitting  $\tau$  in the evaluation of the code length has a small influence on the estimation results, and for brevity we discuss in this study only the predictive approach.

To apply the SC formula from [6] we have to compute the term  $\ln \int_{\Theta} |\mathbf{J}_N(\theta)|^{1/2} d\theta$  for which it is difficult to find a closed-form expression. For the simpler AR case, the integral was evaluated with Monte Carlo techniques in [9]. In our application, a supplementary difficult is due to the application, a supplementary

difficulty is due to the amplitudes  $\alpha_k$ , for which the domain does not have an upper bound. This makes us to prefer the SC formula derived in [8]:

$$SC(y^{N}; K, M) = -\ln f(y^{N}; \hat{\theta}, \hat{\tau}) + \ln |\mathbf{J}_{N}(\hat{\theta})|^{1/2} + \sum_{i=1}^{3K+M} \ln(|\hat{\theta}_{i}| + N^{-1/4})$$
(3)

We check in Appendix how the conditions for the derivations from [8] are fulfilled for the model of sinusoids in Gaussian AR noise. In Appendix we also give more details on the accuracy of the approximation in formula (3).

To gain more insight, we briefly analyze what SC formula (3) becomes for  $N \to \infty$ . Based on the results from the Appendix, we get the well-known asymptotic identity  $\lim_{N\to\infty} \ln |\mathbf{J}_N(\hat{\theta})|^{1/2} = \frac{5K+M}{2} \ln N$ , and it is easy to notice that the sum of the first two terms in SC is equivalent with the Bayesian information criterion (BIC):

$$BIC(y^{N}; K, M) = -\ln f(y^{N}; \hat{\theta}, \hat{\tau}) + \frac{5K + M}{2} \ln N.$$
 (4)

More details on the derivation of BIC can be found in [5] and the references therein. The formula (4) was also obtained in [2] as a crude version of the Minimum Description Length criterion. In [10], the use of the *maximum a posteriori probability* methodology in conjunction with asymptotic approximations led also to (4) for the particular case of white noise.

We focus on the last term in (3), and for simplicity we assume M = 0 (white noise). The two-step encoding procedure adopted in [8] employs first a uniform quantization of  $\Theta$  that is performed with the same precision for all the parameters. The term  $N^{-1/4}$  in (3) is due to the option from [8] to select this precision based on the minimum eigenvalue of FIM. If zero does not belong to the domain of the parameter  $\theta_i$ , then  $\hat{\theta}_i \neq 0$  and  $\ln(|\hat{\theta}_i| + N^{-1/4})$  is much smaller than  $\frac{1}{2} \ln N$  [8]. Hence the term  $\ln(|\hat{\theta}_i| + N^{-1/4})$  becomes important only when  $\hat{\theta}_i = 0$ . Since among the  $\xi$  parameters only the phases can be equal to zero, asymptotically the penalty term in SC formula takes values between  $\frac{9K}{4} \ln N$  and  $\frac{5K}{2} \ln N$ . Based on this observation, it is easy to show that the necessary conditions for consistency from [11] are verified.

#### **3. COMPUTATIONAL ISSUES**

The use of (3) is very appealing from computational viewpoint, but it was already pointed out in [8] that (3) is not invariant under re-

SC	Hypothesis	$\mathbf{J}_N(\xi)$	$\mathbf{J}_N(\mathfrak{g})$
SCp	Hrp	exact	exact
SCa	H <sub>rp</sub> /Ĥ <sub>dp</sub>	asymptotic	asymptotic
SCe	H <sub>dp</sub>	exact	exact

 Table 1. Nomenclature for SC when various formulae for FIM are used in calculations.

parametrization. Due to this reason, we prefer to use as parameters for the AR noise the magnitudes and angles of the poles instead of the coefficients.

More precisely, let us assume that the poles of the AR noise are  $g_1, \ldots, g_M$ : if the poles  $g_1, \ldots, g_{M_1}$  are real-valued, then the pure complex poles  $g_{M_1+1}, \ldots, g_M$  occur in complex conjugate pairs because the coefficients a are real-valued. Instead of  $\theta = (\xi, \mathfrak{a})$ , we will apply the parametrization  $\eta = (\xi, \mathfrak{g})$ , where

 $\mathfrak{g} = (g_1, \ldots, g_{M_1}, |g_{M_1+1}|, \psi_{g_{M_1+1}}, \ldots, |g_{M-1})|, \psi_{g_{M-1}})$  and for a complex pole  $g_i$ , the symbol  $\psi_{g_i}$  denotes its angle. Remark the range of the entries of  $\mathfrak{g}$ : we have  $g_i \in (-1, 1)$  for  $1 \leq i \leq M_1$ , and for the rest of the parameters  $|g_i| \in (0, 1)$  and  $\psi_{g_i} \in (0, \pi)$ .

In [1], it is proven that  $|\mathbf{J}_N(\eta)|$  can be factorized as  $|\mathbf{J}_N(\xi)| \times |\mathbf{J}_N(\mathfrak{g})|$ , where the block  $\mathbf{J}_N(\xi)$  corresponds to the signal parameters, and the block  $\mathbf{J}_N(\mathfrak{g})$  corresponds to the noise parameters. The reference [1] gives also fast algorithms for the evaluation of  $\mathbf{J}_N(\xi)$ .  $\mathbf{J}_N(\mathfrak{g})$  has the same expression as in the pure AR case, and for its calculation we resort to the exact and asymptotic formulae from [12]. We note that the formulae are given for the a parameters and their change to  $\mathfrak{g}$  parameters is straightforward [13].

Applying the exact or asymptotic formulae for  $J_N(\xi)$  and  $J_N(\mathfrak{g})$  leads to various expressions for SC. In Table 1, we explain the nomenclature for SC when FIM in (3) is evaluated with various formulae.

#### 4. EXPERIMENTAL RESULTS

In all the examples presented next, we resort to the RELAX algorithm that performs a decoupled parameter estimation for the sinusoids and the AR noise [3]. In our simulations we have used for the implementation of RELAX Matlab functions that are publicly available at *http://www.uni-kassel.de/fb16/hfk/neu/toolbox*.

Asymptotically both RELAX and ML yield statistically efficient estimates, and the use of RELAX is recommended due to its lower computational burden [3][4].

For  $\gamma = (K, M)$ , let  $\hat{\xi}_k$  be the parameters of the k-th sinusoid estimated with RELAX. We denote  $\hat{e}_t = y_t - \sum_{k=1}^{K} \hat{\alpha}_k \cos(\hat{\omega}_k t + \hat{\phi}_k)$ , and let  $\hat{a}$  be the coefficients of the AR noise determined from the sequence  $\hat{e}_0, \ldots, \hat{e}_{N-1}$ . We further define the residual sum of squares as  $\text{RSS}_{\gamma} = \sum_{t=0}^{N-1} \left[ \hat{e}_t + \sum_{m=1}^{M} \hat{a}_m \hat{e}_{t-m} \right]^2$ , with the convention that  $\hat{e}_t = 0$  for t < 0.

In SC formula (3) and the BIC formula (4),  $-\ln f(y^N; \hat{\theta}, \hat{\tau})$  is evaluated as  $\frac{N}{2} \ln RSS_{\gamma}$  after discarding the terms that do not depend on  $\gamma$ . The performances of SC and BIC are compared in our simulations with two other criteria: KICc and GAIC. KICc was derived in [14] as a unbiased Kullback Information Criterion for linear regression models with i.i.d Gaussian noise. Since then its application was extended also to other classes of models, see for example [15] and the references therein. GAIC is a generalized Akaike Information Criterion that was traditionally used in conjunction with the RELAX algorithm [3].

Example 1 ( $K = 2$ )							Example $2(K = 2)$										
SNR2=-3.00 dB							SNR <sub>2</sub> =1.00 dB										
N	30	40	50	60	70	80	90	100	N	30	40	50	60	70	80	90	100
SCp	37	69	76	85	98	98	98	95	SCp	36	52	73	73	76	85	85	94
SCa	36	68	73	84	95	95	97	95	SCa	34	45	71	68	75	84	85	94
SCe	31	62	64	77	89	85	90	84	SCe	27	28	68	73	74	85	85	94
BIC	33	50	58	66	83	90	93	96	BIC	6	28	67	67	78	89	89	97
KICc	61	74	77	48	52	51	37	40	KICc	21	23	35	36	32	39	35	44
GAIC	3	1	19	23	44	62	68	80	GAIC	6	8	32	43	61	74	84	97
			SNR	2 = -1.00	dB							SNF	R2=3.00	dB			
N	30	35	40	45	50	60	80	100	N	30	35	40	45	50	60	80	100
SCp	72	86	91	95	97	98	99	99	SCp	57	54	74	83	94	89	95	96
SCa	72	83	84	90	91	98	97	98	SCa	56	52	63	75	90	89	94	96
SCe	58	64	76	77	77	86	89	92	SCe	48	42	17	29	87	85	94	96
BIC	50	05	72	81	82	89	97	99	BIC	31	32	44	59	84	84	97	98
KICC	83	89	81	/9	/4	74	48	44	KICC	38	39	30	38	54	35	44	43
GAIC	>	23	32	48	01	/5	88	100	GAIC	11	/	15	21	51	00	90	98
N	25	20	25	2=0.00	45 45	50	75	100	N	25	20	25	40	dB 45	50	75	100
IN SCa	23	30	33	40	4.5	30	7.5	100	IN SCn	2.5	50	33	40	43	50	/3	100
SCp	70	80	90	95	90	90	96	97	SCp	49	62	68	/0 61	74	87	95	98
SCa	56	67	70	83 74	04 75	90	95	97	SCa	29	54	45	14	15	87	92	98
BIC	52	54	70	75	97	00	02	100	BIC	22	25	51	47	91	82	95	100
KICc	79	81	91	87	81	76	55	33	KICc	38	32	44	30	42	50	40	43
GAIC	10	24	36	46	65	70	98	100	GAIC	13	18	27	31	62	77	100	100
one	1 10				0.0			100	0.110		10	~ /		02		100	100
			E	2/1/	0)				1			F	L 4 ( TZ	0)			
			Exampl	$e_{3(K)}$	= 2)							Examp	le 4 (K)	= 3			
N	20	40	Exampl SNR	e 3 (K) $1^{=1.00}$	= 2) dB	80	00	100	N	20	40	Examp SNR	1e 4 (K) 1=-5.00	= 3) ) dB	80	00	100
N	30	40	Example SNR 50	e 3 (K 1=1.00 60	= 2) dB 70	80	90	100	N	30	40	Examp SNR 50	1e 4 (K) 1=-5.00 60 71	= 3) dB 70 76	80	90	100
N SCp SCa	30 74 71	40 74	Example SNR 50 88 81	e 3 (K 1=1.00 60 89 85	= 2) dB 70 <b>80</b> 77	80 79	90 81 81	100 91 87	N SCp SCa	30 21 21	40 75 75	Examp SNR 50 76 77	le 4 (K) 1=-5.00 60 71 71 71	= 3) ) dB 70 76 77	80 76 76	90 85 85	100 85 84
N SCp SCa SCe	30 74 71 64	40 74 65 69	Example SNR 50 88 81 80	e 3 (K 1=1.00 60 89 85 89	= 2) dB 70 80 77 80	80 79 77 79	90 81 81 80	100 91 87 91	N SCp SCa SCe	30 21 21 35	40 75 75 66	Examp SNR 50 76 77 72	le 4 (K) 1=-5.00 60 71 71 68	= 3) ) dB 70 76 77 72	80 76 76 76	90 85 85 84	100 85 84 83
N SCp SCa SCe BIC	30 74 71 64 42	40 74 65 69 56	Example SNR 50 88 81 80 70	e 3 (K 1=1.00 60 89 85 89 77	= 2) dB 70 80 77 80 73	80 79 77 79 73	90 81 81 80 72	100 91 87 91 82	N SCp SCa SCe BIC	30 21 21 35 19	40 75 75 66 60	Examp SNR 50 76 77 72 72 72	1 = -5.00 60 71 71 68 67	= 3) 0 dB 70 76 77 72 73	80 76 76 76 67	90 85 85 84 79	100 85 84 83 76
N SCp SCa SCe BIC KICc	30 74 71 64 42 60	40 74 65 69 56 68	Example SNR 50 88 81 80 70 70 70	e 3 (K 1=1.00 60 89 85 89 77 61	= 2) dB 70 80 77 80 73 58	80 79 77 79 73 51	90 81 81 80 72 48	100 91 87 91 82 51	N SCp SCa SCe BIC KICc	30 21 21 35 19 52	40 75 75 66 60 68	Examp SNR 50 76 77 72 72 61	1e 4 (K) 1=-5.00 60 71 71 68 67 56	= 3) 0 dB 70 76 77 72 73 56	80 76 76 76 67 47	90 85 85 84 79 53	100 85 84 83 76 39
N SCp SCa SCe BIC KICc GAIC	30 74 71 64 42 60 13	40 74 65 69 56 68 41	Example SNR 50 88 81 80 70 70 63	e 3 (K 1=1.00 60 89 85 89 77 61 68	= 2) dB 70 80 77 80 73 58 74	80 79 77 79 73 51 71	90 81 81 80 72 48 72	100 91 87 91 82 51 80	N SCp SCa SCe BIC KICc GAIC	30 21 21 35 19 <b>52</b> 0	40 75 75 66 60 68 7	Examp SNR 50 76 77 72 72 61 25	$ \frac{1 = -5.00}{60} $ 71 71 68 67 56 44	= 3) 0 dB 70 76 77 72 73 56 65	80 76 76 76 67 47 62	90 85 85 84 79 53 72	100 <b>85</b> 84 83 76 39 71
N SCp SCa SCe BIC KICc GAIC	30 74 71 64 42 60 13	40 74 65 69 56 68 41	Example SNR 50 88 81 80 70 70 63 SN	e 3 (K 1=1.00 60 89 85 89 77 61 68 R1=3.0	= 2) dB 70 <b>80</b> 77 <b>80</b> 73 58 74 0	80 79 77 79 73 51 71	90 81 81 80 72 48 72	100 91 87 91 82 51 80	N SCp SCa SCe BIC KICc GAIC	30 21 21 35 19 <b>52</b> 0	40 75 75 66 60 68 7	Examp SNR 50 76 77 72 72 61 25 SNR	$ \frac{1}{60} = -5.00 \\  \hline  \hline $	= 3) 0 dB 70 76 77 72 73 56 65 0 dB	80 76 76 67 47 62	90 85 85 84 79 53 72	100 <b>85</b> 84 83 76 39 71
N SCp SCa SCe BIC KICc GAIC	30 74 71 64 42 60 13 30	40 74 65 69 56 68 41 35	Example SNR 50 88 81 80 70 70 63 80 70 63 80 80 80 80 80 80 80 80 80 80 80 80 80	$ \begin{array}{r}         e 3 (K) \\         1 = 1.00 \\         \hline         60 \\         89 \\         85 \\         89 \\         77 \\         61 \\         68 \\         R_1 = 3.0 \\         45 \\         \end{array} $	= 2) dB 70 <b>80</b> 77 <b>80</b> 73 58 74 0 50	80 79 77 79 73 51 71 60	90 81 81 80 72 48 72 48 72 80	100 91 87 91 82 51 80 100	N SCp SCa SCe BIC KICc GAIC	30 21 21 35 19 <b>52</b> 0	40 75 75 66 60 68 7 40	Examp SNR 50 76 77 72 72 61 25 61 25 SNR 50	$ \frac{1}{60} = \frac{4 (K)}{60} = \frac{60}{71} = \frac{60}{71} = \frac{60}{56} = \frac{60}{44} = \frac{60}{60} = \frac{1}{60} = \frac{60}{60} = \frac{1}{60} $		80 76 76 76 67 47 62 80	90 85 85 84 79 53 72 90	100 <b>85</b> 84 83 76 39 71
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N SCp SCa SCe BIC KICc GAIC N SCp SCa	30 74 71 64 42 60 13 30 <b>84</b> 74	40 74 65 69 56 68 41 35 <b>89</b> 82	Exampl SNR 50 88 81 80 70 70 63 SN 40 93 85	$\begin{array}{c} e \ 3 \ (K) \\ 1 = 1.00 \\ \hline 60 \\ 89 \\ 85 \\ 89 \\ 77 \\ 61 \\ 68 \\ \hline R_1 = 3.0 \\ \hline 45 \\ \hline 82 \\ 74 \end{array}$	= 2) dB 70 <b>80</b> 77 <b>80</b> 73 58 74 0 50 <b>88</b> 85	80 79 77 79 73 51 71 60 87 <b>88</b>	90 81 80 72 48 72 80 85 82	100 91 87 91 82 51 80 100 82 80	N SCp SCa BIC KICc GAIC N SCp SCa	30 21 21 35 19 <b>52</b> 0 30 35 35	40 75 75 66 60 68 7 40 85 <b>86</b>	Examp SNR 50 76 77 72 72 61 25 SNR 50 82 82	$ \frac{ e \ 4 \ (K) }{1 = -5.00} \\ \frac{60}{71} \\ \frac{71}{68} \\ \frac{67}{56} \\ \frac{44}{1 = -3.00} \\ \frac{60}{91} \\ \frac{91}{91} $	= 3) 0 dB 70 76 77 72 73 56 65 0 dB 70 88 88	80 76 76 67 47 62 80 90 89	90 85 85 84 79 53 72 90 90 96 96	100 <b>85</b> 84 83 76 39 71 100 <b>90</b> 88
N SCp SCa SCe BIC KICc GAIC O N SCp SCa SCa	30 74 71 64 42 60 13 30 <b>84</b> 74 72	40 74 65 69 56 68 41 35 <b>89</b> 82 77	Exampl SNR 50 88 81 80 70 70 63 SN 40 93 85 81	$\begin{array}{c} \mathbf{e} \ 3 \ (K) \\ 1 = 1.00 \\ 60 \\ 89 \\ 85 \\ 89 \\ 77 \\ 61 \\ 68 \\ 81 = 3.0 \\ 45 \\ 82 \\ 74 \\ 76 \end{array}$	= 2) dB 70 80 77 80 73 58 74 0 50 88 85 85	80 79 77 79 73 51 71 60 87 <b>88</b> 86	90 81 80 72 48 72 80 85 82 85	100 91 87 91 82 51 80 100 82 80 82	N SCp SCa SCe BIC KICc GAIC N SCp SCa SCe	30 21 21 35 19 52 0 30 35 35 52	40 75 75 66 60 68 7 40 85 <b>86</b> 78	Examp SNR 50 76 77 72 72 61 25 SNR 50 82 82 75		= 3) 0 dB 70 76 77 72 73 56 65 0 dB 70 88 88 88 84	80 76 76 67 47 62 80 90 89 85	90 85 85 84 79 53 72 90 90 96 96 93	100 85 84 83 76 39 71 100 90 88 88
N SCp SCa SCe BIC KICc GAIC GAIC N SCp SCa SCe BIC	30 74 71 64 42 60 13 30 30 84 74 72 49	40 74 65 69 56 68 41 35 89 82 77 64	Example SNR 50 88 81 80 70 63 81 80 70 63 81 85 81 77	$\begin{array}{c} \hline e \ 3 \ (K) \\ \hline 1 = 1.00 \\ \hline 60 \\ \hline 89 \\ 85 \\ 89 \\ 77 \\ 61 \\ 68 \\ \hline R_1 = 3.0 \\ \hline 45 \\ \hline 82 \\ 74 \\ 76 \\ 68 \end{array}$	= 2) dB 70 80 77 80 73 58 74 0 50 88 85 85 77	80 79 77 79 73 51 71 60 87 88 86 82	90 81 81 80 72 48 72 48 72 80 80 85 82 85 79	100 91 87 91 82 51 80 100 82 80 82 82 87	N SCp SCa SCc BIC KICc GAIC GAIC N SCp SCa SCc BIC	30 21 21 35 19 <b>52</b> 0 30 35 35 52 27	40 75 75 66 60 68 7 40 85 <b>86</b> 78 80	Examp SNR 50 76 77 72 72 61 25 SNR 50 82 82 75 77	$\begin{array}{c} \begin{array}{c} 1 = -5.00 \\ \hline 0 \\ \hline 0 \\ \hline 71 \\ -71 \\ -68 \\ -7 \\ -56 \\ -44 \\ \hline 1 = -3.00 \\ \hline 60 \\ \hline 91 \\ -85 \\ -83 \\ \end{array}$	= 3) 0 dB 70 76 77 72 73 56 65 0 dB 70 88 88 88 84 84	80 76 76 67 47 62 80 80 90 89 85 83	90 85 85 84 79 53 72 90 90 96 96 93 92	100 <b>85</b> 84 83 76 39 71 100 <b>90</b> 88 86 <b>90</b>
N SCp SCa SCe BIC KICc GAIC N SCp SCa SCe BIC KICc	30 74 71 64 42 60 13 30 84 74 72 49 74	40 74 65 69 56 68 41 35 89 82 77 64 79	Example SNR 50 88 81 80 70 70 63 SN 40 93 85 81 77 83	$\begin{array}{c} \hline {\bf e} \ 3 \ (K) \\ \hline {\bf 1} = 1.00 \\ \hline {\bf 60} \\ \hline {\bf 89} \\ 85 \\ {\bf 89} \\ 77 \\ 61 \\ 68 \\ \hline {\bf R1} = 3.0 \\ \hline {\bf 45} \\ \hline {\bf 82} \\ 74 \\ 76 \\ 68 \\ 72 \end{array}$	= 2) dB 70 80 77 80 73 58 74 0 50 50 88 85 85 77 71	80 79 77 79 73 51 71 60 87 88 86 82 69	90 81 81 80 72 48 72 48 72 80 85 79 59	100 91 87 91 82 51 80 100 82 80 82 87 40	N SCp SCa SCe BIC KICc GAIC N SCp SCa SCe BIC KICc	30 21 21 35 19 <b>52</b> 0 30 35 35 52 27 <b>69</b>	40 75 75 66 60 68 7 40 85 <b>86</b> 78 80 84	Examp SNR 50 76 77 72 61 25 SNR 50 82 82 75 77 71	$\begin{array}{c} \begin{array}{c} 1 = -5.00 \\ \hline 0 \\ \hline 0 \\ \hline 71 \\ 71 \\ 68 \\ 67 \\ 56 \\ 44 \\ \hline 1 = -3.00 \\ \hline 60 \\ \hline 91 \\ 85 \\ 83 \\ 71 \end{array}$	= 3) 0 dB 70 76 77 72 73 56 65 0 dB 70 <b>88</b> <b>88</b> <b>84</b> 84 58	80 76 76 67 47 62 80 80 89 85 83 56	90 85 85 84 79 53 72 90 90 96 96 93 92 55	100 85 84 83 76 39 71 100 90 88 86 90 48
N SCp SCa SCe BIC KICc GAIC N SCp SCa SCe BIC KICc GAIC	30 74 71 64 42 60 13 30 84 74 72 49 74 49	40 74 65 69 56 68 41 35 89 82 77 64 79 52	Example SNR 50 88 81 80 70 63 70 63 81 85 81 77 83 74	$\begin{array}{c} \hline {e\ 3\ }(K \\ 1 = 1.00 \\ \hline 60 \\ \hline 89 \\ 85 \\ 89 \\ 77 \\ 61 \\ 68 \\ \hline R_1 = 3.0 \\ 45 \\ \hline 82 \\ 74 \\ 76 \\ 68 \\ 72 \\ 78 \\ \end{array}$	= 2) dB 70 <b>80</b> 77 <b>80</b> 73 58 74 0 50 <b>88</b> 85 85 77 71 83	80 79 77 79 73 51 71 71 60 87 88 86 82 69 86	90 81 81 80 72 48 72 72 80 85 85 82 85 79 59 80	100 91 87 91 82 51 80 100 82 80 82 80 82 87 40 91	N SCp SCa SCe BIC KICC GAIC N SCp SCa SCe BIC KICC GAIC	30 21 21 35 19 <b>52</b> 0 35 35 35 52 27 <b>69</b> 0	40 75 75 66 60 68 7 7 40 85 <b>86</b> 78 <b>86</b> 78 80 84 29	Examp SNR 50 76 77 72 61 25 SNR 50 82 82 75 77 71 57	le 4 (K)           1=-5.00           60           71           68           67           56           44           1=-3.00           60           91           85           83           71           61	= 3) 0 dB 70 76 77 72 73 56 65 0 dB 70 <b>88</b> <b>88</b> <b>84</b> 58 72	80 76 76 67 47 62 80 89 85 83 56 65	90 85 85 84 79 53 72 90 90 96 93 92 55 80	100 <b>85</b> 84 83 76 39 71 100 <b>90</b> 88 86 <b>90</b> 48 82
N SCp SCa SCe BIC KICc GAIC N SCp SCa SCe BIC KICc GAIC	30 74 71 64 42 60 13 30 84 74 72 49 74 49 74 49	40 74 65 69 56 68 41 35 <b>89</b> 82 77 64 79 52	Exampl SNR 50 88 81 80 70 70 63 81 80 85 81 77 83 74 SNR	$\begin{array}{c} \hline {\bf e} \ 3 \ (K \\ 1 = 1.00 \\ \hline {\bf 60} \\ \hline {\bf 89} \\ 85 \\ {\bf 89} \\ 77 \\ 61 \\ 68 \\ \hline {\bf R1} = 3.0 \\ \hline {\bf 45} \\ \hline {\bf 82} \\ 74 \\ 76 \\ 68 \\ 72 \\ 78 \\ \hline {\bf 1} = 5.00 \\ \end{array}$	= 2) dB 70 <b>80</b> 77 <b>80</b> 73 58 74 0 50 <b>88</b> 85 85 77 71 83 dB	80 79 77 79 73 51 71 60 87 <b>88</b> 86 82 69 86	90 81 81 80 72 48 72 80 85 85 82 85 79 59 80	100 91 87 91 82 51 80 100 82 80 82 80 82 87 40 91	N SCp SCa SCc BIC KICc GAIC N SCp SCa SCa SCa BIC KICc GAIC	30 21 21 35 19 <b>52</b> 0 35 35 35 52 27 <b>69</b> 0	40 75 75 66 60 68 7 7 40 85 <b>86</b> 78 <b>86</b> 78 80 84 29	Examp SNR 50 76 77 72 61 25 61 25 80 82 75 77 71 57 57 SNR	$\begin{array}{r} \hline e \ 4 \ (K \\ 1 = -5.00 \\ \hline 60 \\ \hline 71 \\ 68 \\ 67 \\ 56 \\ 44 \\ \hline 1 = -3.00 \\ \hline 60 \\ \hline 91 \\ 91 \\ 85 \\ 83 \\ 71 \\ 61 \\ \hline 1 = -1.00 \\ \end{array}$	= 3) 0 dB 70 76 77 72 73 56 65 0 dB 70 <b>88</b> <b>88</b> <b>84</b> 58 72 0 dB	80 76 76 76 67 47 62 80 80 89 85 83 56 65	90 85 85 84 79 53 72 90 90 96 93 92 55 80	100 <b>85</b> 84 83 76 39 71 100 <b>90</b> 88 86 <b>90</b> 48 82
N           SCp           SCa           SCe           BIC           KICc           GAIC           N           SCp           SCa           SCp           SCp           SCp           SCp           SCp           SCc           BIC           KICc           GAIC           N	30 74 71 64 42 60 13 30 84 74 72 49 74 49 74 49 25	40 74 65 69 56 68 41 35 <b>89</b> 82 77 64 79 52 30	Exampl SNR 50 88 81 80 70 70 63 81 83 85 81 77 83 85 81 77 83 74 83 5		= 2) dB 70 80 73 58 74 0 50 50 85 85 85 85 77 71 83 dB 45	80 79 77 79 73 51 71 60 87 88 86 82 69 86 50	90 81 81 80 72 48 72 48 72 80 85 85 82 85 79 59 80 75	100 91 87 91 82 51 80 100 82 80 80 82 87 40 91 100	N SCp SCa SCe BIC KICc GAIC N SCp SCa SCe BIC KICc GAIC N	30 21 21 35 19 <b>52</b> 0 30 35 35 52 27 <b>69</b> 0 30	40 75 75 66 60 68 7 40 85 <b>86</b> 78 80 84 29 35	Examp SNR 50 76 77 72 61 25 81 25 82 75 77 71 57 57 81 82 75 77 71 57 81 840	$\begin{array}{c} \hline \mathbf{k} & 4 & (K \\ 1 & \mathbf{-5.00} \\ \hline & 60 \\ \hline & 71 \\ 71 \\ 68 \\ 67 \\ 56 \\ 44 \\ 1 & \mathbf{-3.00} \\ 60 \\ \hline & 91 \\ 85 \\ 83 \\ 71 \\ 61 \\ 1 & \mathbf{-1.00} \\ 45 \end{array}$	= 3) 0 dB 70 76 77 72 73 56 65 0 dB 70 70 <b>88</b> <b>88</b> <b>84</b> 84 84 84 84 50 50	80 76 76 67 47 62 80 90 89 85 83 56 65 60	90 85 85 84 79 53 72 90 96 96 96 93 92 55 80	100 <b>85</b> 84 83 76 39 71 100 <b>90</b> 88 86 <b>90</b> 48 82 100
N           SCp           SCa           SCe           BIC           KICc           GAIC           N           SCp           SCa           SCc           BIC           KICc           GAIC	30 74 71 64 42 60 13 30 84 74 72 49 74 49 74 49 74 90	40 74 65 69 56 68 41 35 89 82 77 64 79 52 30 93	Example SNR 50 88 81 80 70 70 63 63 85 81 77 83 85 81 77 83 74 83 74 90		= 2) dB 70 80 73 58 74 0 50 85 85 85 85 77 71 83 dB 45 97	80 79 77 79 73 51 71 60 87 88 86 82 69 86 82 69 86 9 50 95	90 81 81 80 72 48 72 48 72 80 85 85 85 85 79 59 80 75 90	100 91 87 91 82 51 80 100 82 80 82 87 40 91 100 90	N SCp SCa SCe BIC KICc GAIC N SCp SCa SCe BIC KICc GAIC N SCp	30 21 21 35 19 <b>52</b> 0 30 35 35 52 27 <b>69</b> 0 30 30 41	40 75 75 66 60 68 7 40 85 86 78 80 84 29 35 85	Examp SNR 50 76 77 72 72 61 25 50 82 82 82 82 82 82 75 77 71 57 75 77 71 57 80R 40 <b>93</b>	$\begin{array}{c} \hline \mathbf{k} 4 \ (K \\ 1 = -5.00 \\ \hline 60 \\ \hline 71 \\ 71 \\ 68 \\ 67 \\ 56 \\ 44 \\ 1 = -3.00 \\ \hline 60 \\ 91 \\ 85 \\ 83 \\ 71 \\ 61 \\ 1 = -1.00 \\ \hline 45 \\ \hline 89 \\ \end{array}$	= 3) 0 dB 70 76 77 72 73 56 65 0 dB 70 <b>88</b> <b>88</b> <b>84</b> 84 84 58 72 0 dB 50 <b>93</b>	80 76 76 67 47 62 80 89 85 83 56 65 60 93	90 85 85 84 79 53 72 90 90 96 96 93 92 55 80 80 80 94	100 <b>85</b> 84 83 76 39 71 100 <b>90</b> 88 86 <b>90</b> 48 82 
N SCp SCa SCe BIC KICc GAIC N SCp SCa SCe BIC KICc GAIC N SCp SCa	30 74 71 64 42 60 13 30 84 74 72 49 74 49 74 49 74 85	40 74 65 69 56 68 41 35 89 82 77 64 79 52 30 93 87	Example SNR 50 88 81 80 70 70 63 63 80 80 80 85 81 77 83 74 83 74 83 74 83 74 83 84	$\begin{array}{c} \mathbf{e} \ 3 \ (K \\ 1 = 1.00 \\ 60 \\ 89 \\ 85 \\ 89 \\ 77 \\ 61 \\ 68 \\ \mathbf{R_1} = 3.0 \\ 45 \\ 82 \\ 74 \\ 76 \\ 68 \\ 72 \\ 78 \\ 1 = 5.00 \\ 40 \\ 91 \\ 91 \end{array}$	= 2) dB 70 80 73 58 73 58 70 50 88 85 85 77 71 83 dB 45 97 81	80 79 77 79 73 51 71 60 87 88 86 82 69 86 69 86 50 95 92	90 81 80 72 48 72 80 85 85 85 85 79 59 80 75 90 86	100 91 87 91 82 51 80 100 82 80 82 87 40 91 100 90 90	N SCp SCa SCe BIC KICc GAIC N SCp SCa BIC KICc GAIC N SCp SCa SCe Ca SCe Ca SCe SCe SCa SCe SCe SCe SCe SCe SCe SCe SCe SCe SCe	30 21 21 35 19 <b>52</b> 0 35 35 52 27 <b>69</b> 0 30 30 41 40	40 75 66 60 68 7 40 85 86 78 80 84 29 35 85 85 85	Examp SNR 50 76 77 72 72 61 25 SNR 50 <b>82</b> 82 82 82 75 77 71 57 71 57 81 82 82 82 82 82 82 82 82 82 82 82 82 82	le 4 (K           1=-5.00           60           71           71           68           67           56           44           1=-3.00           91           91           85           83           71           61           1=-1.00           45           89           89	= 3) 0 dB 70 76 77 72 73 56 0 dB 70 88 88 84 58 72 0 dB 50 93 91	80 76 76 67 47 62 80 90 89 85 83 56 65 65 60 93 91	90 85 85 84 79 53 72 90 96 96 93 92 55 80 80 80 94 90	100 85 84 83 76 39 71 100 90 88 88 86 90 48 88 82 100 86 82
N           SCp           SCc           BIC           KICc           GAIC           N           SCp           SCc           BIC           KICc           GAIC           N           SCc           BIC           KICc           GAIC           N           SCp           SCp           SCp           SCc           SCc           SCc	30           74           71           64           42           60           13           30           84           74           74           74           74           74           74           74           74           74           74           74           74           74           74           79           90           85           79	40 74 65 69 56 68 81 35 89 82 77 64 79 52 30 30 93 87 78	Exampl SNR 50 88 80 70 63 SN 40 93 85 81 77 83 74 SNR 35 90 84 74 74	$\begin{array}{c} \mathbf{e} \ 3 \ (K \\ 1 = 1.00 \\ 60 \\ 89 \\ 85 \\ 89 \\ 77 \\ 61 \\ 68 \\ \mathbf{R_1} = 3.0 \\ 45 \\ 82 \\ 74 \\ 76 \\ 68 \\ 72 \\ 78 \\ 1 = 5.00 \\ 40 \\ 91 \\ 77 \\ 83 \\ 77 \\ 83 \\ 77 \\ 83 \\ 77 \\ 83 \\ 77 \\ 83 \\ 77 \\ 83 \\ 77 \\ 83 \\ 77 \\ 83 \\ 77 \\ 83 \\ 77 \\ 83 \\ 77 \\ 83 \\ 77 \\ 83 \\ 77 \\ 83 \\ 77 \\ 83 \\ 77 \\ 83 \\ 77 \\ 77 \\ 83 \\ 77 \\ 87 \\ 77 \\ 87 \\ 87 \\ 77 \\ 87 \\ 77 \\ 87 \\ 77 \\ 87 \\ 77 \\ 87 \\ 77 \\ 77 \\ 87 \\ 77 \\ 77 \\ 87 \\ 77 \\ 77 \\ 87 \\ 77 \\ 77 \\ 87 \\ 77 \\ 77 \\ 87 \\ 77 \\ 77 \\ 87 \\ 77$	= 2) dB 70 80 73 58 74 0 50 88 85 85 77 71 83 dB 45 90	80 <b>79</b> 77 <b>79</b> 73 51 71 <b>60</b> <b>87</b> <b>88</b> 86 82 69 86 <b>85</b> <b>95</b> <b>95</b> <b>92</b> <b>93</b>	90 81 80 72 48 72 80 85 85 85 79 59 80 75 90 86 88	100 91 87 91 82 51 80 100 82 80 82 87 40 91 100 90 90 88	N SCp SCa SCe BIC KICc GAIC N SCp SCa SCe BIC KICc KICc GAIC N N SCp SCa SCe	30 21 21 35 19 <b>52</b> 0 35 35 35 52 27 <b>69</b> 0 30 41 40 50	40 75 75 66 60 68 7 7 40 85 86 78 80 84 29 35 85 85 65	Examp SNR 50 76 77 72 72 61 25 SNR 50 82 82 75 77 71 57 71 57 SNR 40 92 92 86	le 4 ( <i>K</i> 1=-5.00 60 71 68 67 56 44 1=-3.00 60 91 85 83 71 61 1=-1.00 45 89 71	= 3) 0 dB 70 76 77 72 73 56 65 0 dB 70 <b>88</b> <b>88</b> <b>88</b> <b>84</b> 84 84 84 84 50 0 dB 70 77 77 70 77 70 70 77 70 70	80 76 76 67 47 62 80 89 89 85 83 56 55 65 65 90 93 91 82	90 85 85 84 79 90 96 96 93 92 55 80 80 94 90 86	100 85 84 83 76 39 71 100 90 88 86 86 90 48 82 100 86 82 85
N SCp SCa SCe BIC KICC GAIC N SCp SCa SCe BIC KICC GAIC N N SCp SCa SCe BIC BIC	30           74           71           64           42           60           13           30           84           74           79           52	40 74 65 69 56 68 41 35 <b>89</b> 82 77 64 79 52 30 <b>93</b> 87 78 60	Exampl SNR 50 88 81 80 70 63 SN 40 93 85 81 77 83 74 SNR 35 90 84 4 67	e 3 (K 1=1.00 60 89 85 89 77 61 68 R1=3.0 45 82 74 76 68 72 78 1=5.00 40 91 77 77 77	= 2) dB 70 80 77 80 73 58 74 0 50 88 85 77 71 83 dB 45 97 81 90 86	80 79 77 73 51 71 60 87 88 86 82 69 86 82 69 86 95 95 92 93 84	90 81 81 80 72 48 72 80 85 85 82 85 79 59 80 75 90 86 88 88 87	100 91 87 91 82 51 80 82 80 82 87 40 91 100 90 90 88 94	N SCp SCa SCc BIC KICc GAIC N SCp SCa SCe BIC KICc GAIC N N SCp SCa SCa BIC BIC	30 21 35 19 52 0 30 35 52 27 69 0 30 41 40 50 33 33	40 75 66 60 68 7 40 85 <b>86</b> 88 80 84 29 35 85 85 85 85 85 85	Examp SNR 50 77 72 25 SNR 50 61 25 SNR 82 82 82 75 77 71 57 71 57 80 82 82 82 82 82 82 82 82 82 82 82 82 82	le 4 ( <i>K</i> 1=-5.00 60 71 68 67 56 64 44 1=-3.00 60 91 91 91 85 83 71 1=-1.00 45 89 89 89 71 86	= 3) 0 dB 70 76 77 72 73 56 65 0 dB 70 <b>88</b> <b>88</b> <b>88</b> <b>84</b> 84 84 84 50 0 dB 70 77 77 77 73 56 65 9 dB 70 70 77 70 77 72 73 56 65 9 dB 70 70 77 70 70 77 70 70 77 70 70	80 <b>76</b> <b>76</b> 67 47 62 <b>80</b> <b>90</b> 89 85 83 56 65 <b>60</b> <b>93</b> 91 82 90	90 85 85 84 79 90 96 96 96 96 96 92 55 80 80 94 90 94 90	100 <b>85</b> 84 83 76 39 71 100 <b>90</b> 88 86 <b>90</b> 48 82 100 86 82 85 96
N           SCp           SCc           BIC           KICc           GAIC           N           SCp           SCc           BIC           KICc           BIC           SCp           SCp           SCc           BIC           BIC           KICc	30           71           64           42           60           13           30           84           74           72           49           25           90           85           79           85           79           89	40 74 65 69 56 68 41 35 <b>89</b> 82 77 64 79 52 <b>30</b> <b>93</b> 87 78 60 <b>93</b>	Exampl SNR 50 88 81 80 70 63 SN 40 93 85 81 77 83 74 SNR 35 90 84 74 84 74 84 74 84 74 85 80 83 83 83 83 83 83 83 83 85 85 85 85 85 85 85 85 85 85	$\begin{array}{c} \mathbf{e} \ 3 \ (K \\ 1 = 1.00 \\ 60 \\ 89 \\ 85 \\ 89 \\ 77 \\ 61 \\ 68 \\ 77 \\ 66 \\ 82 \\ 74 \\ 76 \\ 68 \\ 72 \\ 78 \\ 72 \\ 78 \\ 1 = 5.00 \\ 91 \\ 77 \\ 83 \\ 77 \\ 80 \\ 80 \\ 77 \\ 80 \\ 80 \\ 77 \\ 80 \\$	= 2) dB 70 80 77 80 77 80 77 80 73 58 74 0 58 85 85 85 85 77 71 83 dB 45 97 81 90 86 88	80 79 77 79 73 51 71 60 87 88 86 82 69 86 50 95 92 93 84 80	90 81 81 80 72 48 72 80 85 82 85 82 85 85 82 85 90 80 75 90 86 88 87 58	100 91 87 91 82 51 80 82 80 80 82 87 40 91 100 90 90 88 84 41	N           SCp           SCce           BIC           KICc           GAIC           N           SCp           SCc           BIC           KICc           BIC           KICc           BIC           KICc           BIC           KICc           BIC           KICc           BIC           KICc           BIC           BIC           BIC           KICc	30 21 21 35 19 52 0 35 35 52 27 69 0 30 41 40 50 33 72	40 75 75 66 60 68 7 40 85 <b>86</b> 78 <b>86</b> 78 <b>86</b> 78 84 29 35 <b>85</b> 85 85 65 575 82	Examp SNR 50 76 77 72 25 SNR 50 82 75 77 71 57 71 57 81 82 75 82 82 82 82 82 82 82 82 82 82 82 82 82		= 3) 0 dB 70 76 77 72 73 56 65 0 dB 70 88 88 84 84 84 84 84 84 84 84	80 <b>76</b> <b>76</b> <b>76</b> <b>67</b> <b>67</b> <b>62</b> <b>80</b> <b>90</b> <b>85</b> <b>83</b> <b>85</b> <b>85</b> <b>85</b> <b>85</b> <b>65</b> <b>60</b> <b>93</b> <b>91</b> <b>82</b> <b>90</b> <b>78</b> <b>78</b> <b>78</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>76</b> <b>77</b> <b>76</b> <b>77</b> <b>76</b> <b>77</b> <b>76</b> <b>77</b> <b>77</b> <b>76</b> <b>77</b> <b>76</b> <b>77</b> <b>76</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>77</b> <b>7</b> <b></b>	90 85 85 84 79 53 72 90 96 96 93 92 55 80 80 94 90 86 62	100 <b>85</b> 84 83 76 39 71 100 <b>90</b> 88 86 <b>90</b> 48 82 <b>100</b> 86 82 85 45 45

Table 2. The counts indicate for 100 runs the number of times the number of sinusoids was correctly estimated by each criterion. The best result for each sample size N is represented with bold font.

In our settings, the maximum number of sinusoids is  $K_{max} = 8$ , and the maximum order of the AR process depends on the number of the available measurements:  $M_{max} = \lfloor \ln^2 N \rfloor - 1$ . The formula for  $M_{max}$  is derived from the condition used in [2] to ensure the consistency of the BIC criterion. Supplementarily, each pair (K, M)must verify the inequality 3K + M < N - 2 to be a candidate for the model structure.

Examples 1-3 are taken from [2], where the estimation results are reported only for  $N \ge 128$ . Since our main interest is on small and moderate sample sizes, we evaluate the performances of the information theoretic criteria for  $N \in \{25, \ldots, 100\}$  and various levels of the local SNR. In Examples 1-3, we consider K = 2 sinusoids whose parameters are  $\xi_1 = (2^{1/2}, 1, 0)$  and  $\xi_2 = (2^{-1/2}, 2, 0)$ . The additive noise is generated as follows:

Example 1:  $e_t = \varepsilon_t$  (white noise), Example 2:  $e_t = -0.81e_{t-2} + \varepsilon_t$  (autoregressive noise),

**Example 3**:  $e_t = \varepsilon_t + 1.6\varepsilon_{t-1} + 0.64\varepsilon_{t-2}$  (moving average noise), where  $\varepsilon_t$  is a sequence of i.i.d Gaussian random variables with zero

mean and variance  $\sigma^2$ , which is chosen such that the local SNR's take the desired values. Example 4 is taken from [3] and modified such that the observa-

Example 4 is taken from [5] and modified such that the observations  $y^N$  are real-valued. The number of sinusoids is K = 3 and their parameters are  $\xi_1 = (2, 0.10\pi, 0), \xi_2 = (2, 0.80\pi, 0)$  and  $\xi_3 = (2, 0.84\pi, 0)$ . The noise is simulated by the autoregressive process  $e_t = 0.85e_{t-1} + \varepsilon_t$ , where the significance of  $\varepsilon_t$  is the same as above.

We focus on the capabilities of the tested criteria to estimate correctly the number of sinusoids K. For the Examples 1-4, we

count the number of correct estimates for 100 runs when the local SNR's and the sample size N take various values. The results are reported in Table 2.

Remark that SCp is the best among the SC formulae and its performances are closely followed by SCa. For both SCp and SCa, FIM of the sinusoidal components are decoupled [1], which is a serious computational advantage. From the results reported in [1], we can draw the conclusion that the shape of the noise spectrum has more influence on SCp than on SCa, and this explains the superiority of the SCp criterion. The performances of SCe are very modest because FIM used in SCe can be ill-conditioned for small and moderate sample size when the number of sinusoids is two or larger [1].

When the sample size N is smaller than 80, SCa is superior to BIC and GAIC. This is a straightforward consequence of the asymptotic approximations applied in the derivations of the BIC and GAIC criteria. KICc estimates for the number of sinusoids are remarkably correct when  $N \leq 40$ , but the number of correct estimations yield by KICc declines when N increases such that for  $N \geq 80$  the reported results are very modest.

We extend our analysis by counting the Type I and Type II errors. Let  $f_k = \omega_k/(2\pi)$  and similarly  $\hat{f}_k = \hat{\omega}_k/(2\pi)$ . Since K and  $\hat{K}$  are not necessarily equal, we take  $\mathcal{K} = \min(K, \hat{K})$ . We select the indices  $\{i_1, \ldots, i_{\mathcal{K}}\} \subseteq \{1, \ldots, K\}$  and  $\{j_1, \ldots, j_{\mathcal{K}}\} \subseteq \{1, \ldots, \hat{K}\}$  such that  $|f_{i_1} - \hat{f}_{j_1}|, \ldots, |f_{i_{\mathcal{K}}} - \hat{f}_{j_{\mathcal{K}}}|$  are the smallest entries of the set  $\{|f_i - \hat{f}_j| : 1 \le i \le K, 1 \le j \le \hat{K}\}$ . For each  $k \in \{1, \ldots, \mathcal{K}\}$ ,  $\hat{f}_{j_k}$  is deemed to be the estimate for  $f_{i_k}$ . As usual, a Type I error is counted in connection with the frequency  $f_k$  if none of the estimated frequencies are assigned to  $f_k$ , and a Type II error is counted whenever  $\hat{K} > K$ . We compute also the mean-squared errors (MSE) for the frequency estimates.

For brevity, we report in Table 3 the Type I and Type II errors together with the MSE only for the experiments conducted in Example 2 when SNR<sub>2</sub>=3.00 dB. In our comparisons, we consider SCp and the asymptotic criteria BIC and GAIC.

We note that only GAIC has difficulties in recovering the first harmonic when N < 50, and recovering the second harmonic whose local SNR is smaller posses problems to all the criteria. Remark for SCp that the number of Type I errors connected with  $f_2$  decreases very fast with the increase of the sample size. For GAIC, the number of Type II errors is always small, but many Type I errors occur even for N = 60. This is a clear sign that, for small N, GAIC underestimates the number of sinusoids. The computed MSE is almost the same for all the investigated criteria and this is natural because the evaluation of SCp, BIC and GAIC is based on the estimates provided by the RELAX algorithm.

**Conclusion** The use of approximations for SC that are sharper than BIC improves the estimation results for small and moderate sample size. The results encourage us to extend the application of SC to other classes of models like 1-D damped harmonics in colored noise, or 2-D sinusoids in white noise.

## Appendix:On the derivation of SC formula (3)

To check the conditions for the applicability of the SC formula of Qian and Künsch in the particular case of the model given by the equations (1) and (2), we resort to a closed-form expression of  $\mathbf{J}_N(\theta)$  that was derived for large sample size [4]. When N is large, under both  $\mathbf{H}_{dp}$  and  $\mathbf{H}_{rp}$ ,  $\mathbf{J}_N(\theta)$  is block-diagonal such that the block

 $\begin{aligned} \mathbf{J}_{N}(\xi_{k}) \text{ corresponds to the parameters of the } k\text{-th sine-wave and the block } \mathbf{J}_{N}(\mathfrak{a}) \text{ corresponds to the parameters of the AR noise [1].} \\ \text{More precisely, we have } \mathbf{J}_{N}(\xi_{k}) = \mathbf{Q}_{N}\mathbf{G}(\xi_{k},\mathfrak{a})\mathbf{Q}_{N}, \text{ where } \mathbf{Q}_{N} = \\ \text{diag}(N^{1/2}N^{3/2}N^{1/2}) \text{ and } \mathbf{G}(\xi_{k},\mathfrak{a}) = \text{SNR}_{k} \begin{bmatrix} 1/\alpha_{k}^{2} & 0 & 0 \\ 0 & 1/3 & 1/2 \\ 0 & 1/2 & 1 \end{bmatrix}. \end{aligned}$ 

Here SNR<sub>k</sub> denotes the local SNR for the k-th sinusoidal component. The entries of  $\mathbf{J}_N(\mathfrak{a})$  are not influenced by the parameters  $\xi$ , hence  $\mathbf{J}_N(\mathfrak{a})$  is the same as in the pure AR case. Based on results from [12] we can write  $\mathbf{J}_N(\mathfrak{a}) = \frac{N}{\tau} \mathbf{R}(\mathfrak{a})$ , where  $\mathbf{R}(\mathfrak{a})$  is the  $M \times M$  covariance matrix of the AR process defined in (2).

After these preliminaries, we outline the conditions as they are given in [8]: (C1)  $\mathbf{J}_N(\theta)$  is positive definite; (C2) The minimum eigenvalue of  $\mathbf{J}_N(\theta)$  is of order O(N) as  $N \to \infty$ ;

(C3)  $|\mathbf{J}_N(\theta_1)|^{-1} ||\mathbf{J}_N(\theta_1)| - |\mathbf{J}_N(\theta_2)|| \le c ||\theta_1 - \theta_2||, \forall \theta_1, \theta_2 \in \Theta,$ where *c* is a finite constant; (C4)  $\ln |\mathbf{J}_N(\theta)| = o(N).$ 

It is easy to check that all the eigenvalues of  $\mathbf{J}_N(\xi_k)$  are strict positive. The covariance matrix  $\mathbf{R}(\mathfrak{a})$  is positive definite for any M, therefore  $\mathbf{J}_N(\mathfrak{a})$  is also positive definite, and the condition C1 is verified. Two of the eigenvalues of  $\mathbf{J}_N(\xi_k)$  are O(N) and the third one is  $O(N^3)$ . As each eigenvalue of  $\mathbf{J}_N(\mathfrak{a})$  is O(N), we conclude that C2 is satisfied. A longer discussion is necessary for C3, but we only remark here that  $|\mathbf{J}_N(\theta)| = N^{5K+M} \frac{|\mathbf{R}(\mathfrak{a})|}{r^M} \prod_{k=1}^K |\mathbf{G}(\xi_k,\mathfrak{a})| \ \forall \theta$ , thus the left-hand-side term in the inequality C3 is finite and does not depend on N. Using the expression above for  $|\mathbf{J}_N(\theta)|$ , we readily obtain  $\lim_{N\to\infty} \frac{\ln |\mathbf{J}_N(\theta)|}{N} = 0$ , thus C4 is verified.

We can apply next the SC formula from [8]. For simplicity we ignore the terms that do not depend on N, and the formula becomes:

 $\begin{aligned} &-\log f(y^{N}; \hat{\theta}, \hat{\tau}) + \log \left| \mathbf{\hat{J}}_{N}(\hat{\theta}, y^{N}) \right|^{1/2} \\ &+ \sum_{i=1}^{3K+M} \log(|\hat{\theta}_{i}| + N^{-1/4}) + \sum_{i=1}^{3K+M} r^{*}(N^{1/4}|\hat{\theta}_{i}| + 1) + O(N^{-1/4}), \\ &\text{where } \log(\cdot) \text{ is the logarithm base } 2, \hat{\theta} \text{ denotes the ML estimates, and} \\ &\mathbf{\tilde{J}}_{N}(\hat{\theta}, y^{N}) = -\frac{\partial^{2} \ln f(y^{N}; \theta, \tau)}{\partial \theta \partial \theta^{\top}} |_{\theta = \hat{\theta}} \text{ is the observed FIM.} \end{aligned}$ 

Frequency $f_1$ : Err. I											
N	30	35	40	45	50	60	80	100			
SCp	2	5	5	0	0	0	0	0			
BIĆ	3	12	15	5	0	0	0	0			
GAIC	28	31	42	26	11	8	0	0			
Frequency $f_1$ : MSE											
N	30	35	40	45	50	60	80	100			
SCp	-59.49	-59.08	-62.82	-63.87	-64.23	-66.57	-75.42	-80.15			
BIČ	-59.78	-59.15	-62.03	-64.57	-64.02	-66.99	-75.42	-80.15			
GAIC	-59.07	-59.96	-62.60	-64.88	-63.58	-67.88	-75.42	-80.15			
	Frequency $f_2$ : Err. I										
N	30	35	40	45	50	60	80	100			
SCp	29	23	12	4	1	0	0	0			
BIĆ	28	29	28	23	4	6	0	0			
GAIC	86	82	79	75	48	32	2	0			
			Freq	uency $f_2$ :	MSE						
N	30	35	40	45	50	60	80	100			
SCp	-50.29	-52.24	-56.82	-55.97	-57.89	-60.81	-63.64	-67.16			
BIČ	-50.67	-39.02	-57.57	-57.70	-57.82	-41.61	-63.56	-67.16			
GAIC	-51.31	-50.60	-58.75	-57.40	-57.28	-40.22	-63.96	-67.16			
Err. II											
N	30	35	40	45	50	60	80	100			
SCp	14	23	14	13	5	11	5	4			
BIČ	41	39	28	18	12	10	3	2			
GAIC	3	11	6	4	1	2	2	2			

**Table 3.** Type I and Type II errors for Example 2 when  $SNR_2=3.00$  dB. MSE is computed for the estimates of the frequencies and it is expressed in dB. The results are reported for 100 runs.

For any x > 0,  $r^*(x) = \log(\log x) + \log(\log(\log x)) + \cdots$ , where the sum continues as long as the iterated logarithms are strict positive.

The approximative formula (3) is obtained from the expression above after replacing  $\mathbf{\tilde{J}}_N(\hat{\theta}, y^N)$  with  $\mathbf{J}_N(\hat{\theta})$ , discarding an

 $O\left((3K+M)\log\log N\right)$  term, and changing  $\log(\cdot)$  to  $\ln(\cdot)$ .

It is recommended in [8] to consider in the SC expression also the term given by the number of parameters divided by two and multiplied by  $\log \rho$ , where  $\rho$  is the largest eigenvalue of  $\mathbf{J}_N(\hat{\theta})^{-1/2} \tilde{\mathbf{J}}_N(\hat{\theta}, y^N) \mathbf{J}_N(\hat{\theta})^{-1/2}$ . It can be readily verified that un-

 $\mathbf{J}_N(\theta)^{-1/2} \mathbf{J}_N(\theta, y^N) \mathbf{J}_N(\theta)^{-1/2}$ . It can be readily verified that under mild conditions  $\rho$  does not depend on N, hence we ignore the  $\log \rho$  term in (3).

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